

Application of UnSWAN for wave hindcasting in the Dutch Wadden Sea

11th Waves Workshop

Marcel Zijlema

October 22, 2009

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Motivation

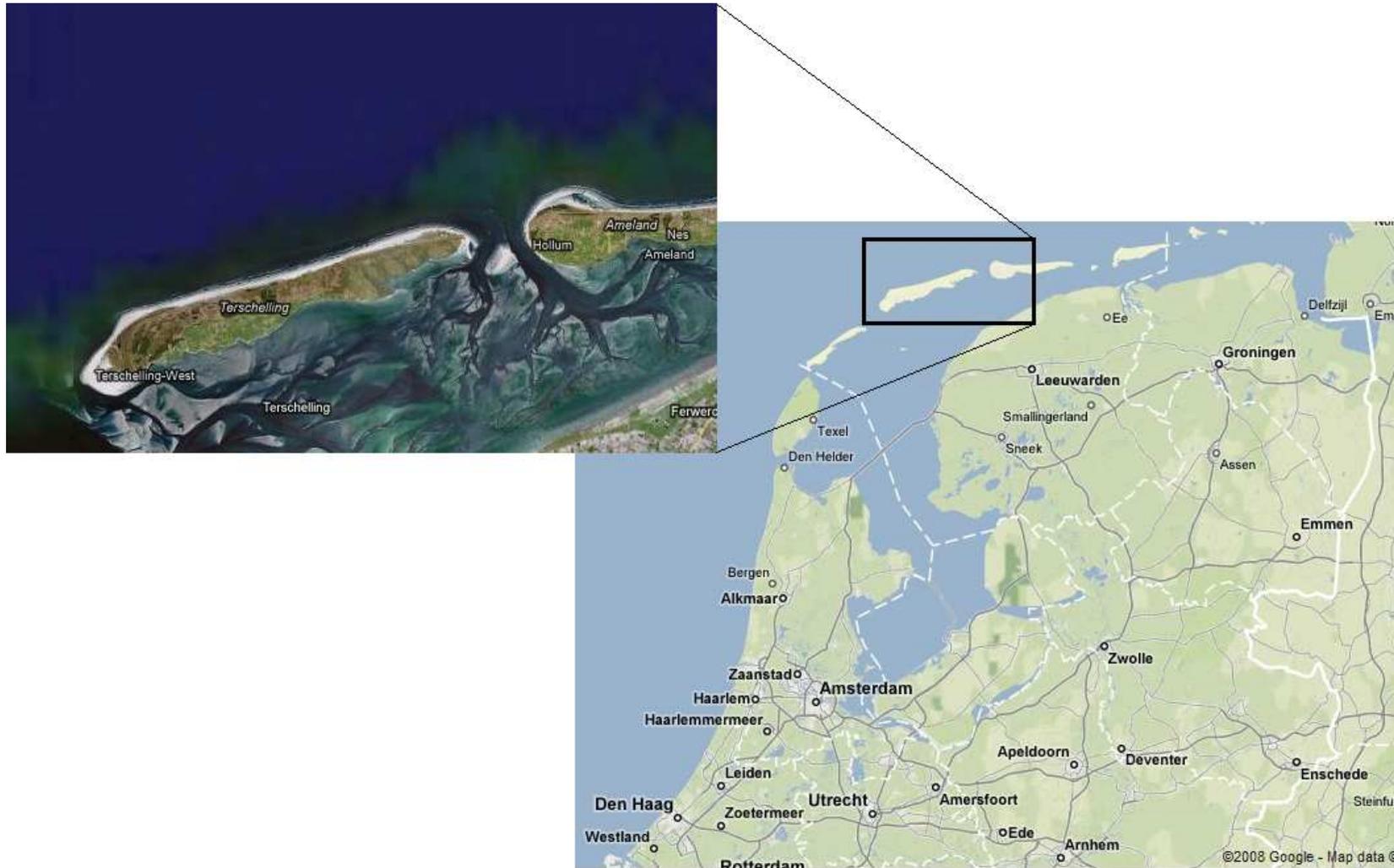
- In the past 10 years, a lot of SWAN studies have been carried out for e.g., the Dutch government
 - main motivations: assessing safety of sea defences and operational wave forecasting
 - studied areas: Scheldt estuaries, lakes (IJsselmeer) and coast (Petten)
 - currently, SBW project initiated at Deltares for studying tidal inlets in the Wadden Sea
- General conclusion: wave heights are good, but wave periods consistently underestimated
- Ask for some improvements in both accuracy and efficiency

Methodology

- The *usual* SWAN approach is a **finite difference, fixed, regular grid** solution to the action balance equation employing the **default third-generation formulations** for deep and shallow water
- Recently, an **unstructured-mesh procedure** is implemented in SWAN
 - Would that be a *better* approach for modelling and understanding wave dynamics in tidal inlets?
- Recently, alternative **source term parameterizations** have been proposed in the literature
 - How about that? Are they useful?

Summary of conclusions

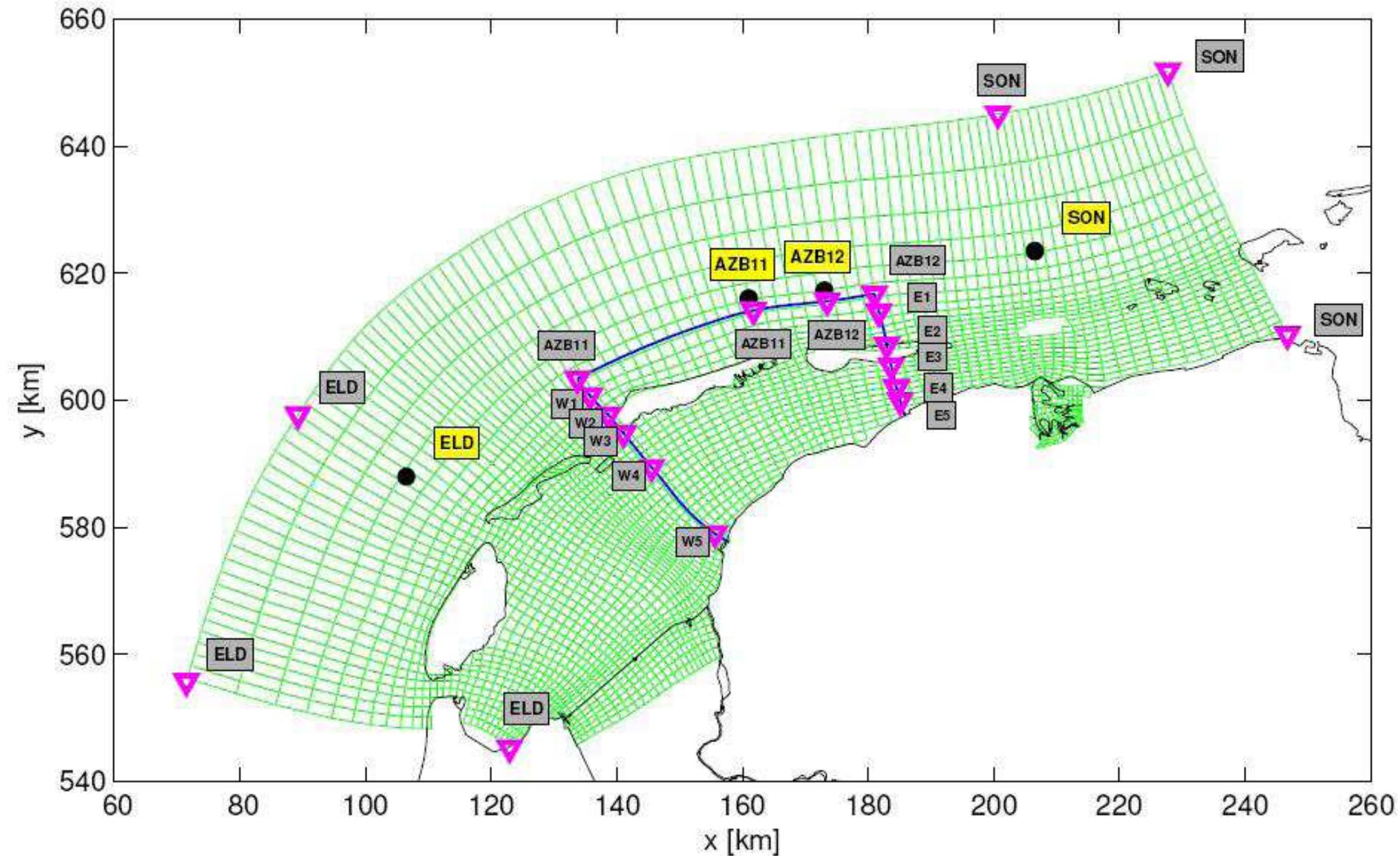
- The parallel, unstructured version of SWAN is a good alternative for tidal inlet studies
 - no nesting and no boundary condition issue
 - achieve good speedups
 - fully compatible with the regular-grid version
- SWAN should be applied with care, choose model settings accordingly
 - optimal settings is found for the Wadden Sea
 - skillful in prediction of wave height and periods over ebb-tidal delta and over shallow interior



Tidal inlet of Ameland connecting the North Sea with the Dutch Wadden Sea

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Nested curvi-linear grids with offshore boundary conditions

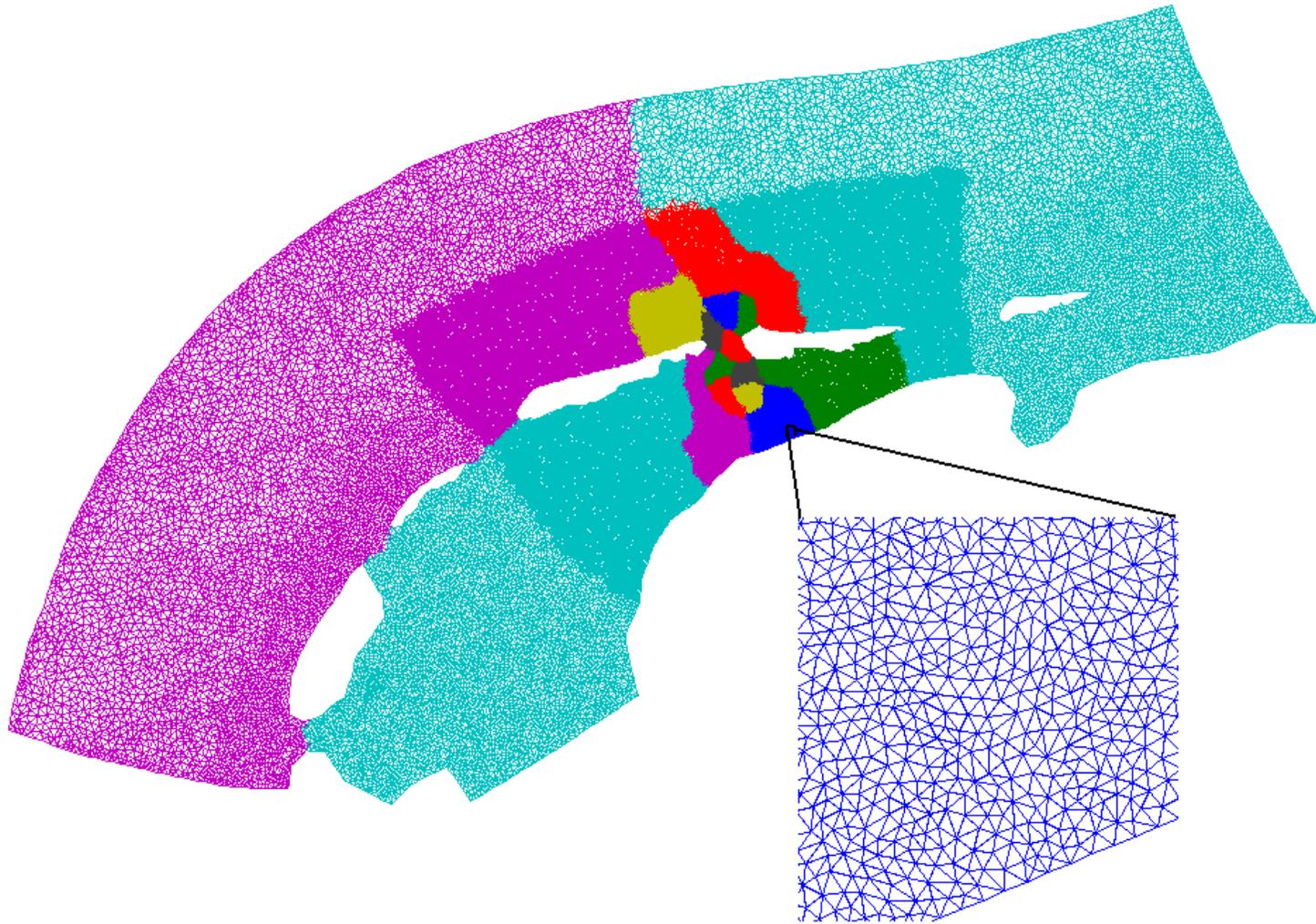
Why unstructured grids?

- Contrary to curvi-linear grids, more flexibility in generating grid as there are no restrictions (smoothness, orthogonality, cell-aspect ratio, etc.)
- Accurate representation of irregular shorelines and islands
- High variability in geographic resolution
- Can take into account large scales in deep water ($\sim 100km$) and small scales in surf zone ($\sim 10m$) in one mesh
- Nested grid problems in terms of correct dynamic coupling and boundary condition discretization accuracy can be avoided

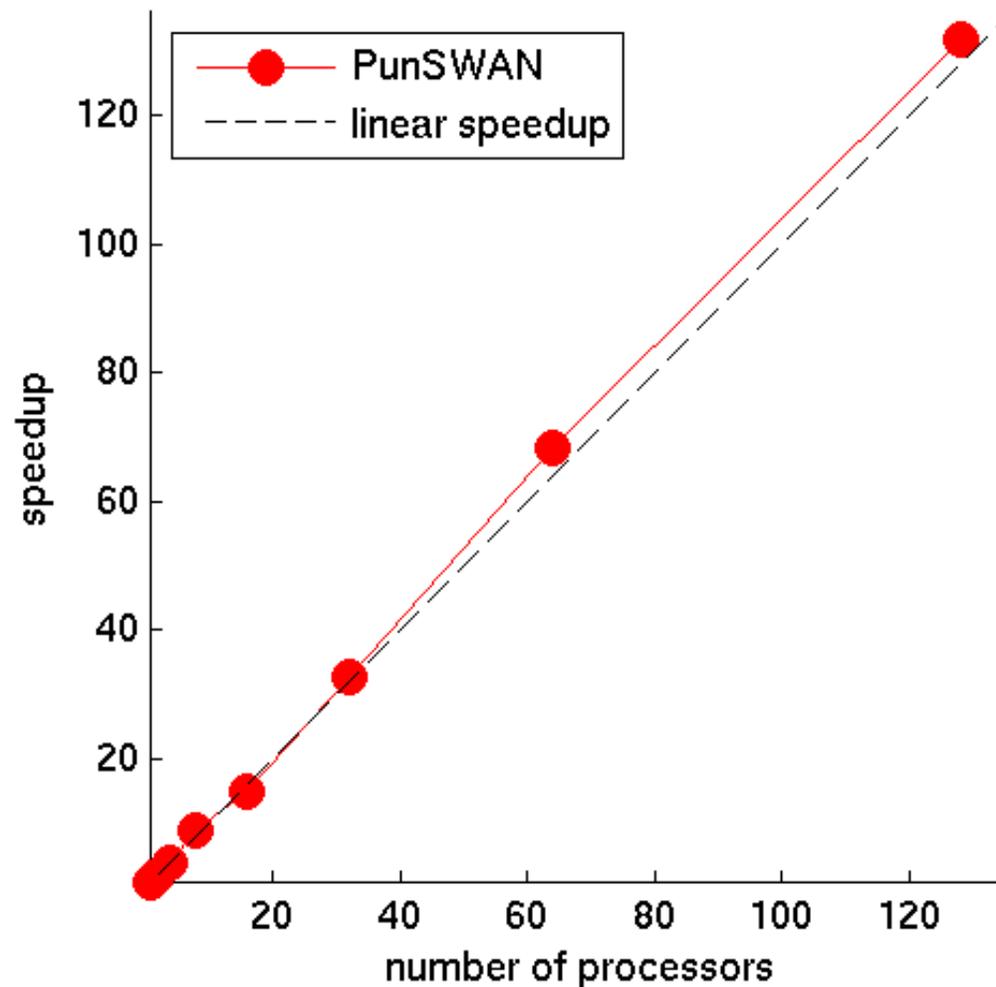
PUnSWAN

- implemented in the ADCIRC environment
- make use of the `adcprep` program:
 - controls domain decomposition for a parallel run
 - **METIS** is called to do the actual grid partitioning
 - creates sub-domain input files after decomposition
- make use of the ADCIRC module `messenger` and **MPI** for
 - local exchanging at subdomain interfaces
 - global reductions e.g., summation, maximum and minimum over all subdomains

Partitioned, unstructured mesh



Parallel efficiency - IBM Power6 cluster



Physics

- General: underprediction of period measures in coastal waters
- Other (more specific) observed inaccuracies in tidal inlets:
 - Underestimation of penetration of low-frequency peak wave energy over ebb-tidal delta
 - Underestimation of finite depth wave growth in near-horizontal beds

Model formulation

- Wave energy represented by action density spectrum $N(x, y, t; \sigma, \theta)$

- Governed by the action balance equation:

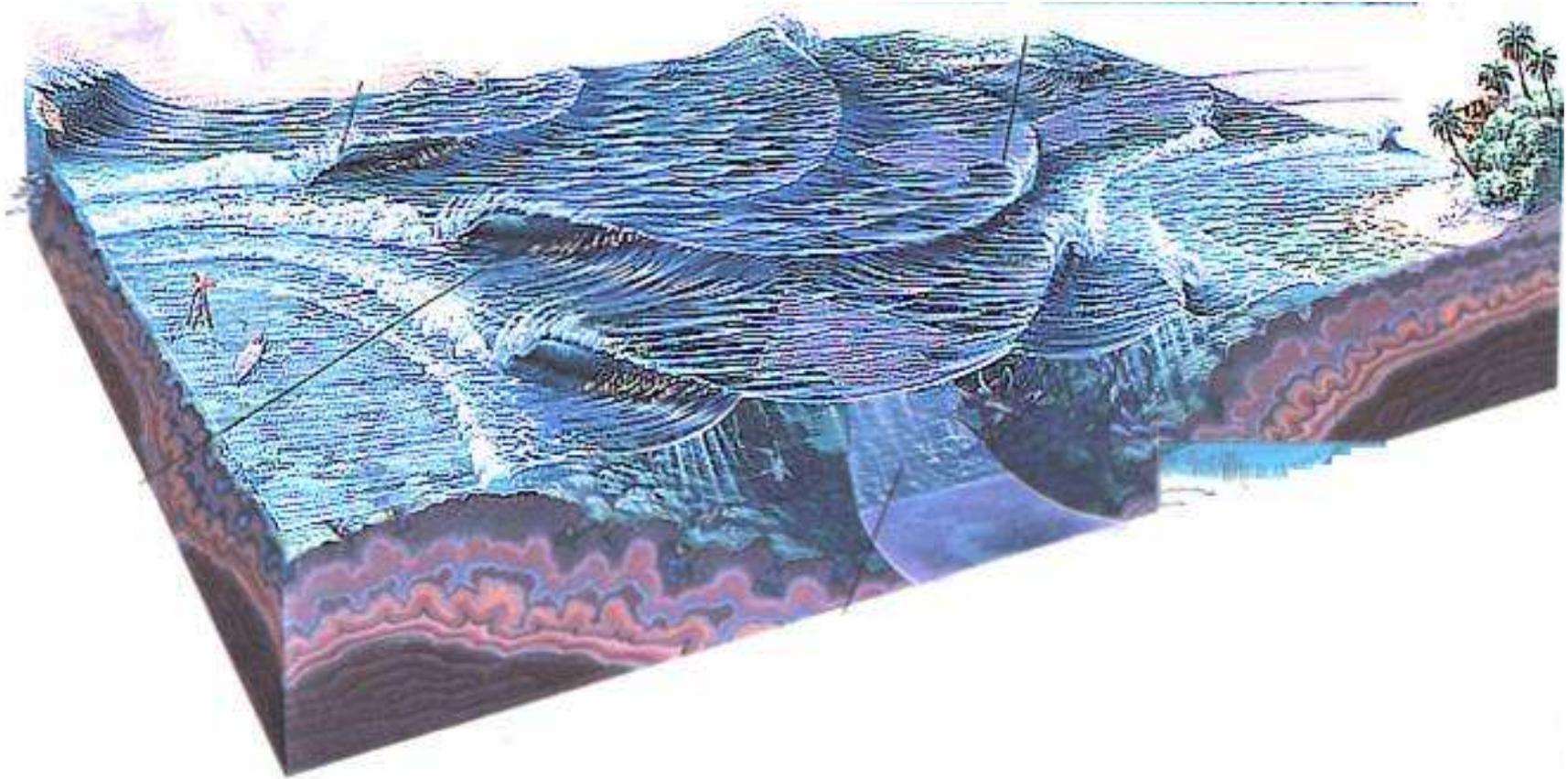
$$\frac{\partial N}{\partial t} + \nabla_{\vec{x}} \cdot [(\vec{c}_g + \vec{U})N] + \frac{\partial c_\sigma N}{\partial \sigma} + \frac{\partial c_\theta N}{\partial \theta} = \frac{S_{\text{tot}}}{\sigma}$$

- Source term S_{tot} describes physical modelling of wave generation, dissipation and redistribution

wind

whitecapping

quadruplets



surf breaking

friction

triads

Whitecapping

Based on Hasselmann (1974) and can be expressed as

$$S_{\text{wcap}} = -C_{\text{ds}} \tilde{\sigma} \left(\frac{\tilde{s}}{\tilde{s}_{\text{pm}}} \right)^m \left(\frac{k}{\tilde{k}} \right)^n E(\sigma, \theta)$$

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$$n = \begin{cases} 1 & \text{Komen et al. (1984)} \\ 2 & \text{Rogers et al. (2003)} \end{cases}$$

The $n = 2$ setting effectively removes underprediction of periods observed with the $n = 1$ setting

Depth-induced breaking (1)

Modelled by the bore-based dissipation model of Battjes and Janssen (1978):

$$S_{\text{brk}} = D_{\text{tot}} \frac{E(\sigma, \theta)}{E_{\text{tot}}}$$

with

$$D_{\text{tot}} = -\frac{1}{4} \alpha_{\text{BJ}} Q_b \left(\frac{\tilde{\sigma}}{2\pi} \right) H_{\text{max}}^2$$

and $\alpha_{\text{BJ}} = 1$ and Q_b is fraction of breaking waves

Depth-induced breaking (2)

The maximum wave height H_{\max} is given by

$$H_{\max} = \gamma_{\text{BJ}} d$$

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where γ_{BJ} is the breaker parameter:

$$\gamma_{\text{BJ}} = \begin{cases} 0.73 & \text{Battjes and Janssen (1978)} \\ 0.76k_p d + 0.29 & \text{Ruessink et al. (2003)} \end{cases}$$

Parameterization of Ruessink et al. (2003) improves finite depth results for a nearly horizontal bed
(Van der Westhuysen, 2009; SBW project)

Bottom friction

Bottom friction is modelled by the JONSWAP formulation (Hasselmann et al., 1973):

$$S_{\text{bot}} = - C_b \frac{\sigma^2}{g^2 \sinh^2(kd)} E(\sigma, \theta)$$

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where C_b is a tunable friction parameter:

$$C_b = \begin{cases} 0.038 m^2 s^{-3} & \text{(swell)} \\ 0.067 m^2 s^{-3} & \text{(fully-developed sea)} \end{cases}$$

Now: $C_b = 0.038 m^2 s^{-3}$ for both swell and **low frequencies in wind-sea spectrum**

Default settings

- Deep water source terms:
 - wind input based on Yan (1987)
 - saturation-based whitecapping of Alves and Banner (2003)
 - DIA for quadruplets (Hasselmann et al., 1985)
- Shallow water source terms:
 - LTA for triads (Eldeberky, 1996)
 - depth-induced breaking: $\gamma_{BJ} = 0.73$ (Battjes and Janssen, 1978)
 - JONSWAP for bottom friction: $C_b = 0.067 m^2 s^{-3}$ (Hasselmann et al., 1973; Bouws and Komen, 1983)

Optimal settings

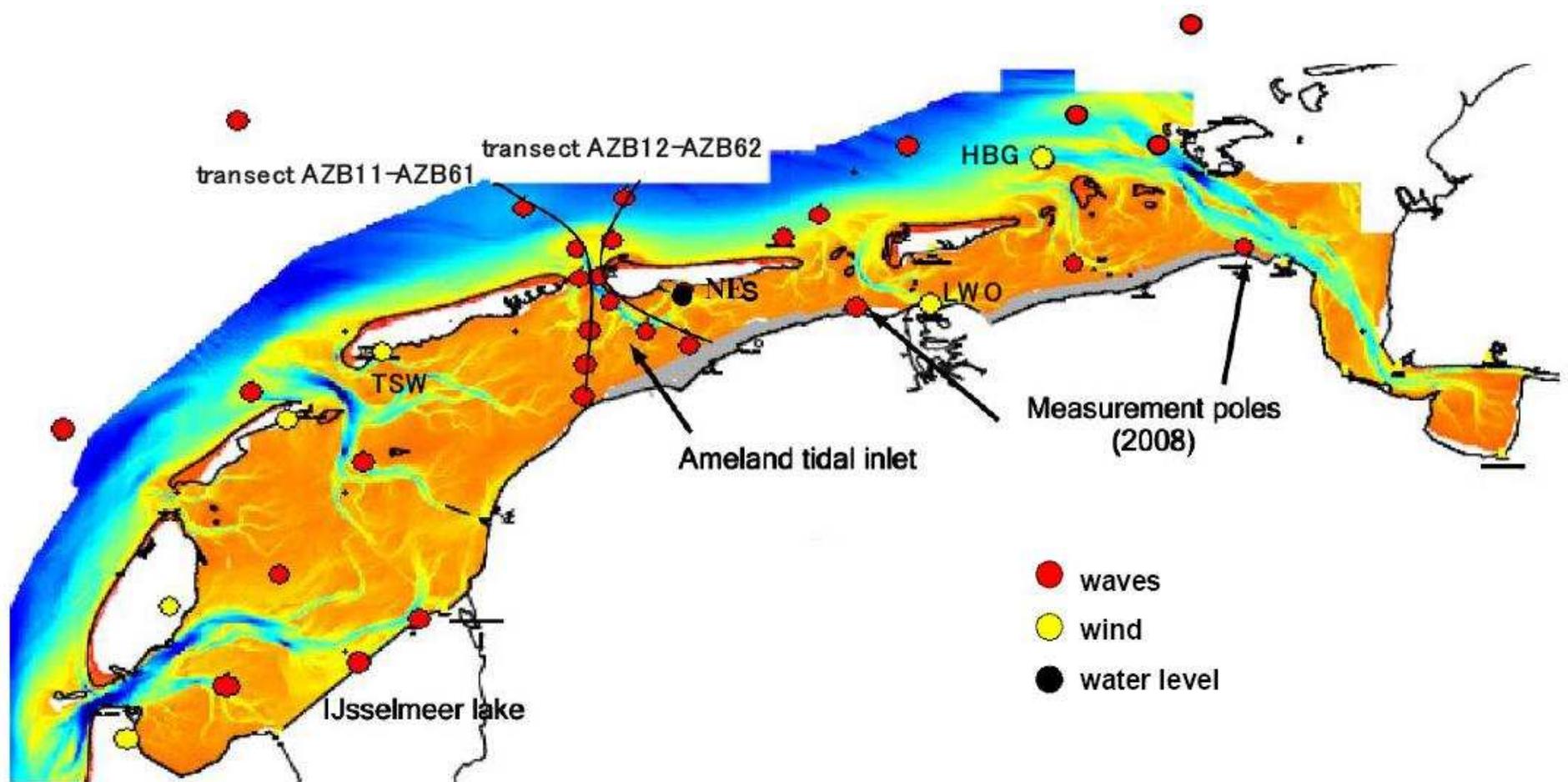
- Deep water source terms:
 - wind input based on Snyder et al. (1981)
 - modified whitecapping expression of Rogers et al. (2003)
 - DIA for quadruplets (Hasselmann et al., 1985)
- Shallow water source terms:
 - switch off LTA triads since transfer to higher frequencies often overestimated
 - depth-induced breaking of BJ78 with breaker index parameterization of Ruessink et al. (2003)
 - JONSWAP for bottom friction: $C_b = 0.038m^2s^{-3}$ (Hasselmann et al., 1973)

Selected storm instants

date and time	U_{10} (m/s)	U_{dir} ($^{\circ}\text{N}$)
11/01/2007, 13h00	19.6	228
11/01/2007, 22h40	19.6	279
18/01/2007, 14h00	20.4	263
18/03/2007, 10h00	14.3	279
18/03/2007, 14h40	18.5	266

These instants are around the peak of the westerly storms with relatively high wind speeds

Measurement locations in Wadden Sea

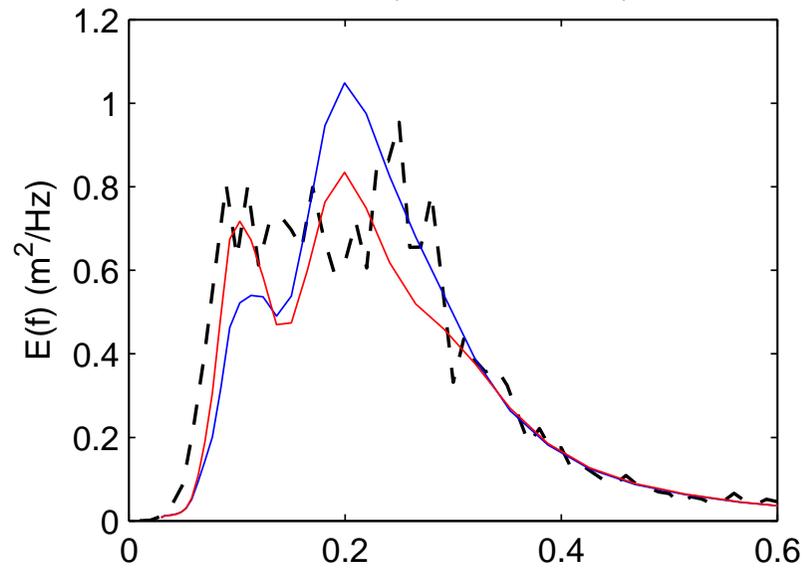


Courtesy of Deltares, The Netherlands

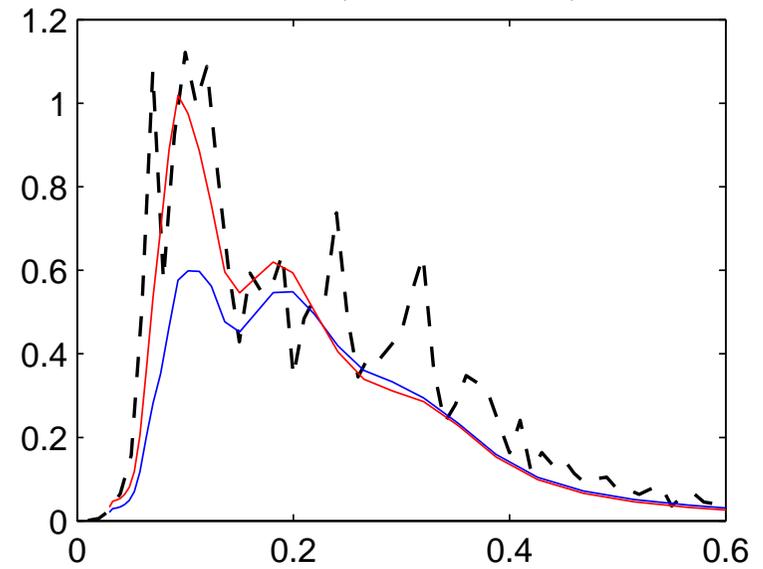
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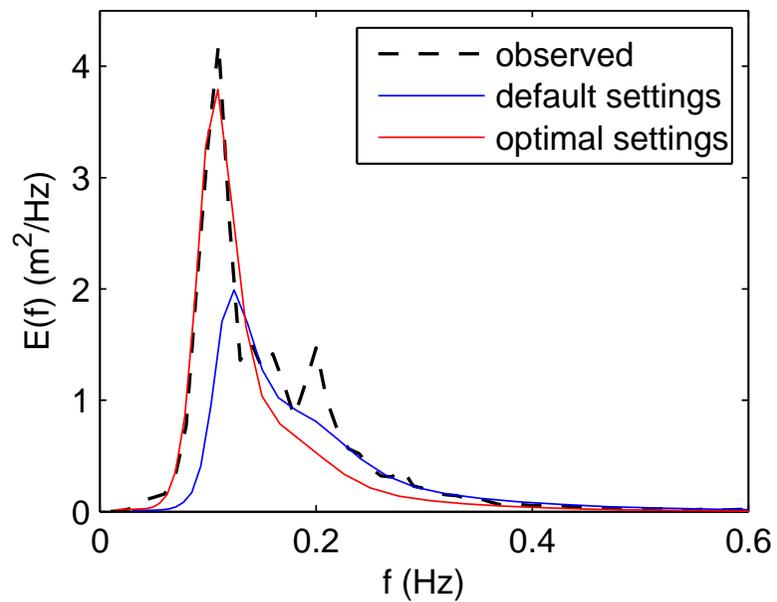
AZB21 (Jan. 11, 13h00)



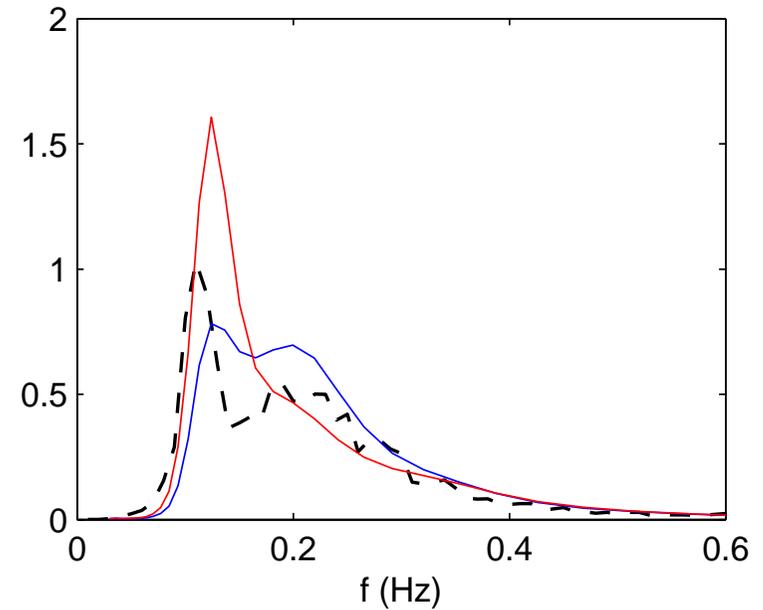
AZB31 (Jan. 11, 13h00)

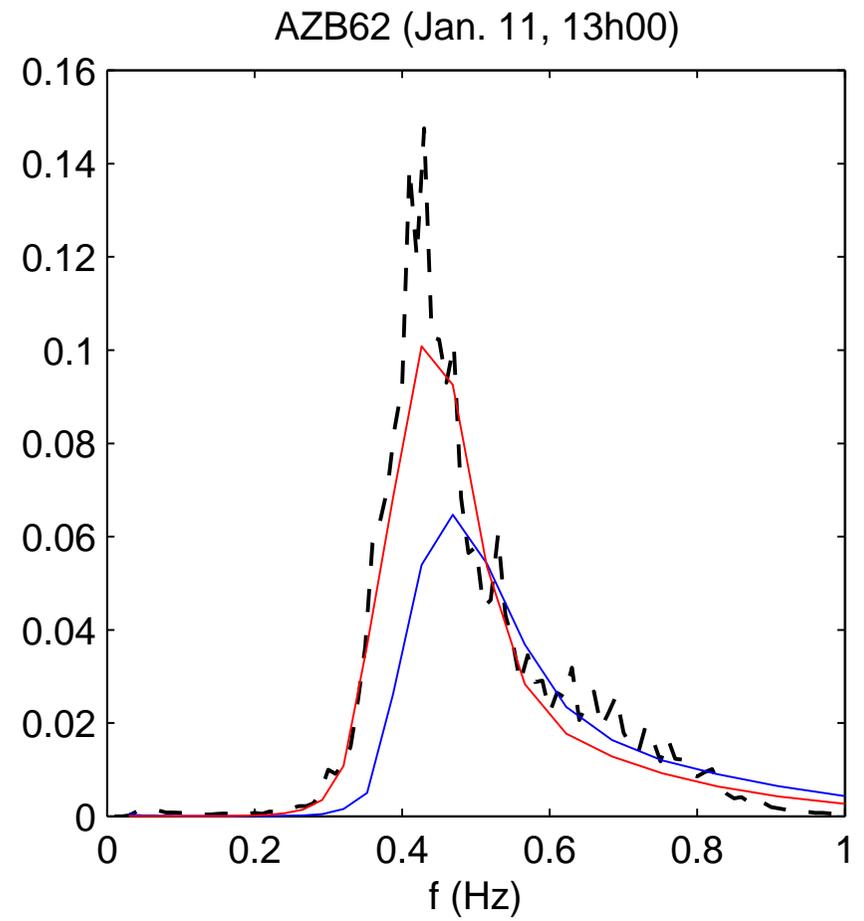
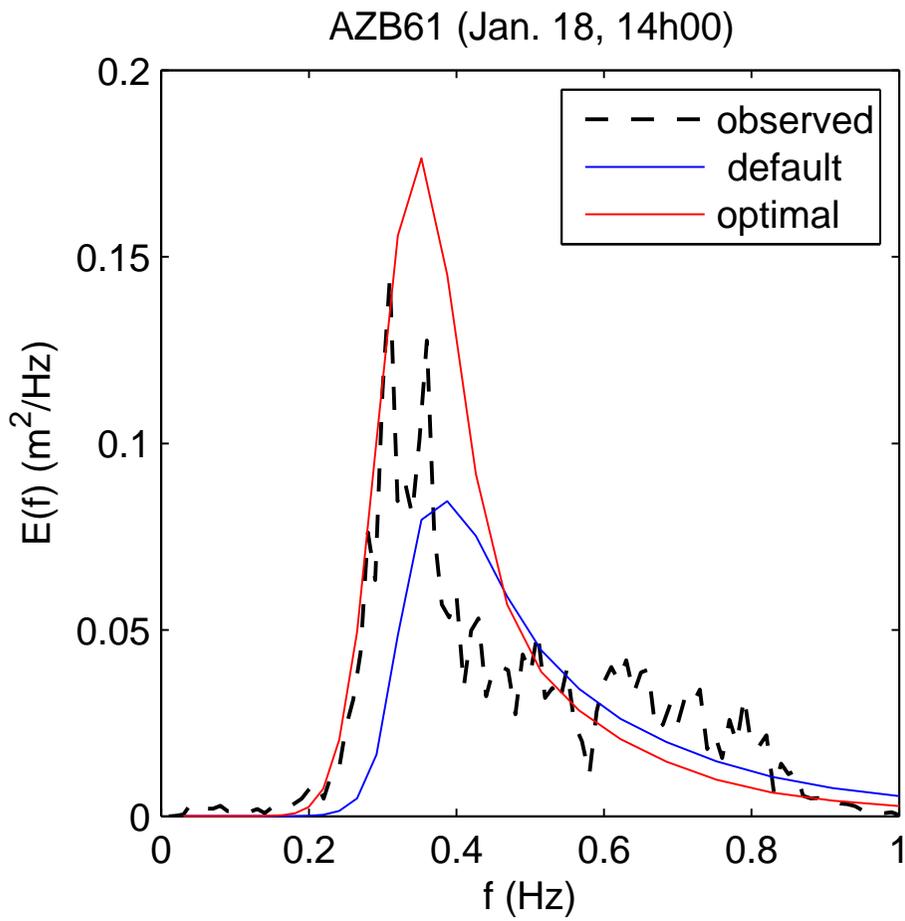


AZB31 (Mar. 18, 10h00)

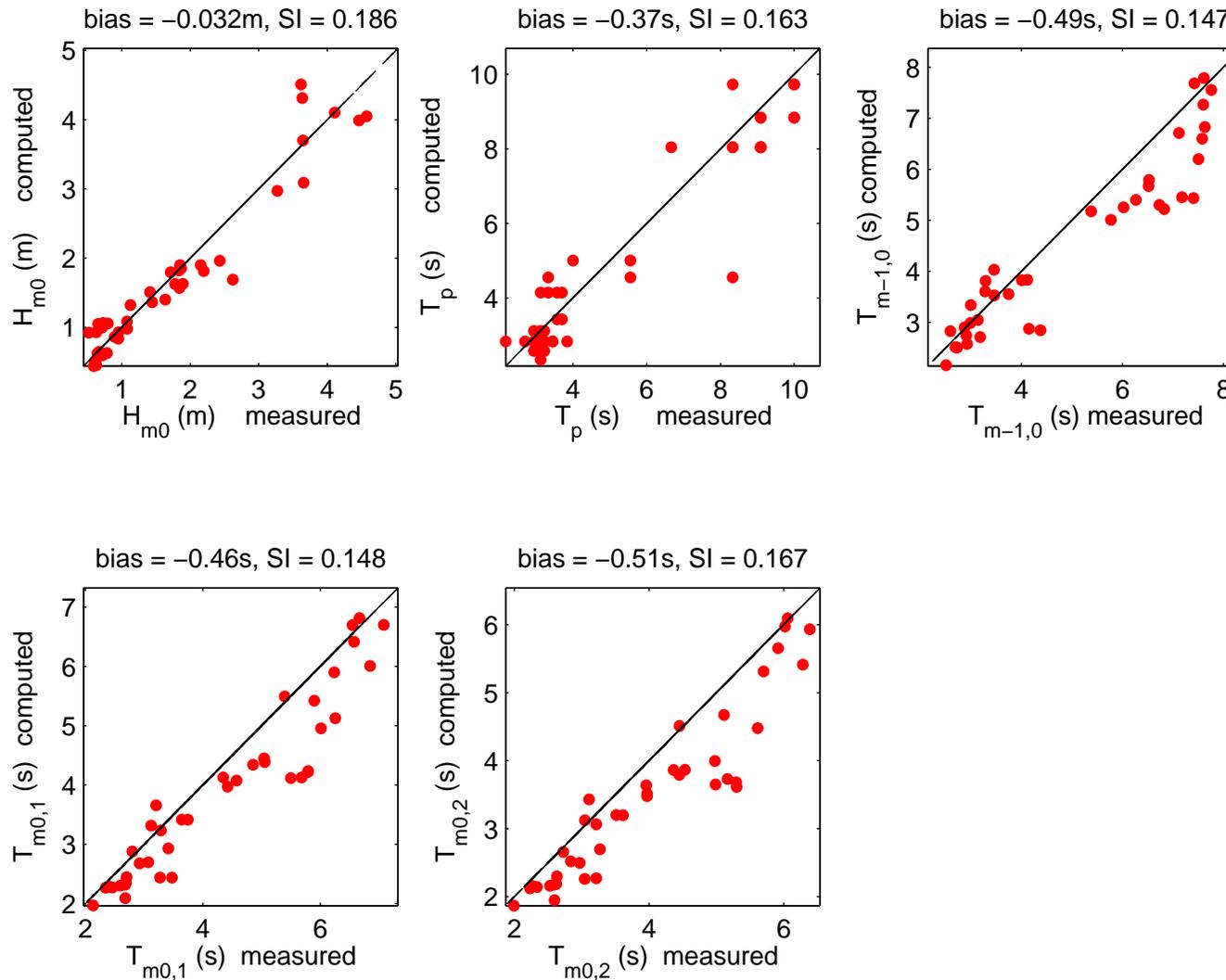


AZB32 (Mar. 18, 10h00)

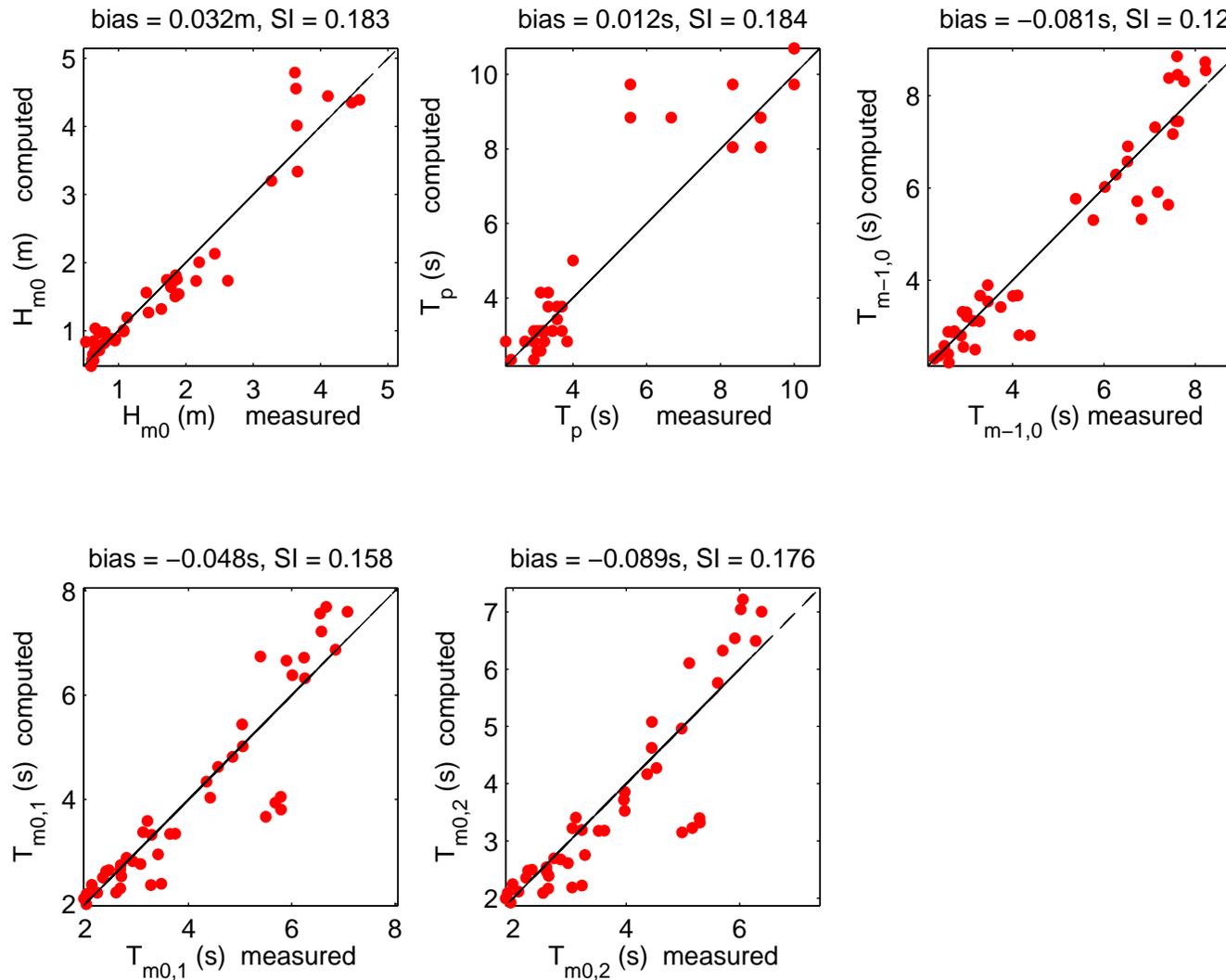


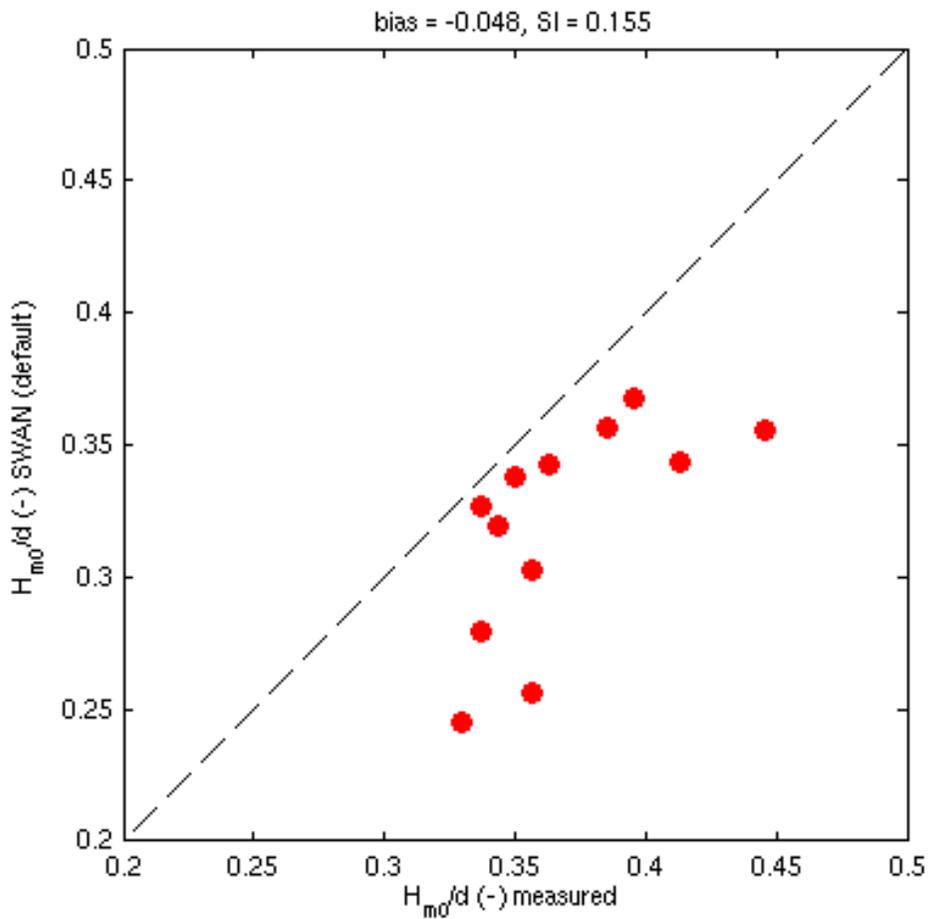


Model vs. measured: default settings

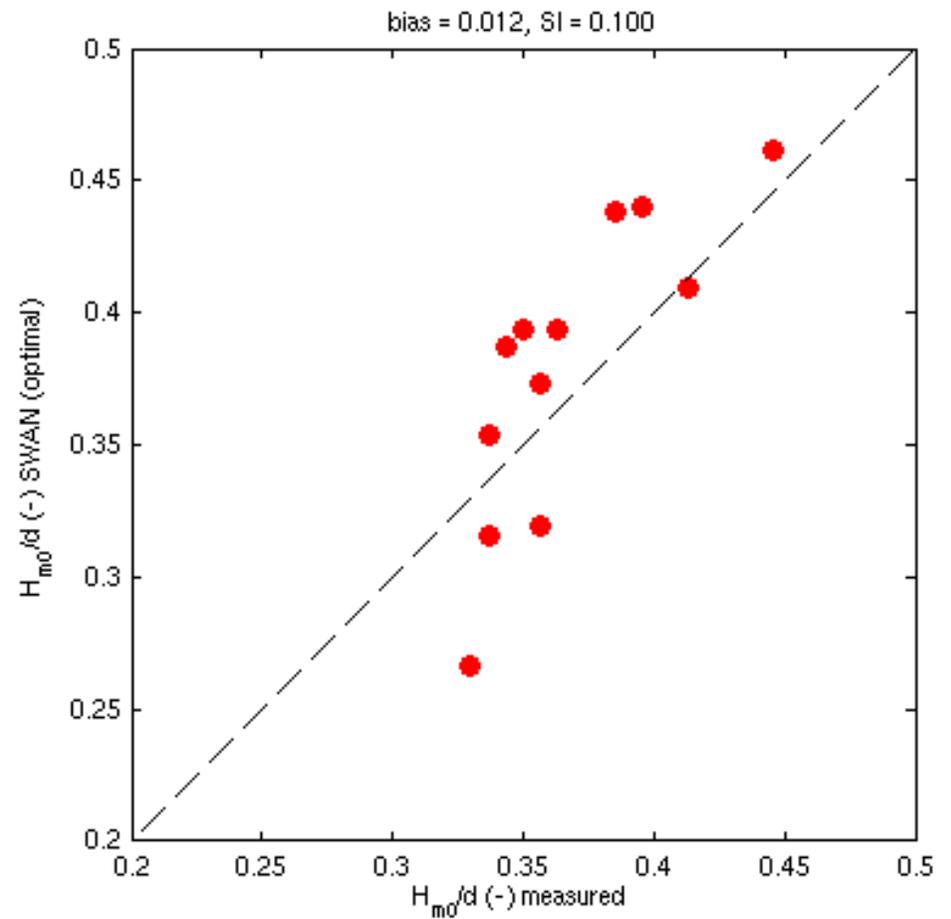


Model vs. measured: optimal settings





default settings



optimal settings

Concluding remarks (1)

- Use of UnSWAN for e.g.,
 - determination of wave climates and
 - hindcasting and forecasting storms
- As computational codes evolve with improvements in computer hardware, we should
 - add new or better **physics** to match the computational capabilities and accuracy
 - develop algorithms to handle **multiscale** physics and increasing **grid resolution**
- More focus on wave features associated with irregular bathymetry, e.g. **surf zones**

Concluding remarks (2)

- A parallel, unstructured version of SWAN has been developed and tested on Linux clusters
- Many known laboratory and field cases have been verified and validated and have shown
 - comparable results to that of regular grids and
 - expected results as indicated by the for SWAN typical bias and SI values
- Achieve good speedups and is scalable
- **UnSWAN** is available in the official release, version 40.72
see website www.swan.tudelft.nl